Angular Distributions from Elastic Scattering of 15-MeV Deuterons*

R. K. Jolly, E. K. Lin, and B. L. Cohen University of Pittsburgh, Pittsburgh, Pennsylvania (Received 8 February 1963)

Angular distributions of 15-MeV deuterons elastically scattered by 23 elements between Al and Pb are presented. A high-resolution detection system provides complete separation from all inelastically scattered deuterons. In light and medium weight elements, there is a sharp diffraction pattern, but it damps out with increasing mass. In a few cases, there are marked differences between angular distributions from nuclei of nearly equal masses.

INTRODUCTION

N recent years, distorted-wave Born approximation calculations have been very successful in analyzing data on various types of direct nuclear reactions. The basic input data for these calculations are the optical model parameters, which are obtained from analyses of elastic scattering angular distributions. Since many of the most useful direct interactions involve deuterons [e.g., (d,p), (d,n), (d,t), (d,α) , (d,Li^{6}) , (p,d), (α,d) , etc.], it is most important to have good data on elastic deuteron scattering over a range of energies.

A rather complete series of measurements of elastic deuteron scattering angular distributions at 11.8 MeV has been reported by Igo *et al.*, 1 and a few results have been reported at 13.0, 13.5, and 15.0 MeV by Cindro and Wall² by the Cracow group³ and by Gofman et al.⁴ at the Institute of Physics of the Academy of Sciences of the Ukrainian S.S.R. We here report a rather extensive study of this type with 15 MeV deuterons. In addition to being more extensive than previous studies, the present work utilizes better energy resolution than the previous work, which is important in some cases.

EXPERIMENTAL PROCEDURE AND ANALYSIS

The scattering facility used in conjunction with the University of Pittsburgh cyclotron has been described in detail previously⁵; it provides focusing and magnetic analysis of the incident deuteron beam, and magnetic analysis of the scattered particles. With its most recent modifications, a continuous range of angles from -30° to $+140^{\circ}$ may be studied, although measurements

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¹G. Igo, W. Lorenz, and U. Schmidt Rohr, Report No. 29 (Max Planck Institute for Nuclear Physics, Heidelberg, Germany, 1961)

² Nikola Cindro and N. S. Wall, Phys. Rev. 119, 1340 (1960). ^a A. Buczanowski and K. Grotowski, Rept. No. 201 (Institute of Nuclear Physics, Cracow, 1962); A. Strzalkowski, Rept. No. 202 (Institute of Nuclear Physics, Cracow, 1962). L. Freindl, H. Nicwodniczanski, J. Nurzynski, M. Slapa, and A. Strzalkowski, Rept. No. 203 (Institute of Nuclear Physics, Cracow, 1962).

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H. Niewodniczanski, J. Nurzynski, and J. Wilczynski, Rept. No. 204 (Institute of Nuclear Physics, Cracow, 1962).
⁴ Y. U. Gofman and O. F. Nemets, Zh. Eksperim. i Teor. Fiz. 39, 1489 (1960) [translation: Soviet Phys.—JETP 12, 1035 (1961)].
⁵ R. S. Bender, E. M. Reilly, A. J. Allen, R. Ely, J. S. Arthur, and H. J. Hausmann, Rev. Sci. Instr. 23, 542 (1952).

beyond 90° require a time consuming change of scattering chambers.

In the present experiment, the scattered particles are detected on the focal plane of the reaction product magnetic analyzing system by a triple scintillator apparatus shown in Fig. 1. It consists of three thin CsI (Tl) scintillation crystals, two 1/8-in.-wide "side" crystals on each side of the 1/4-in.-wide "center" crystal. In measuring the count rate of elastically scattered deuterons, the magnetic field is varied until practically all counts come from the center crystal and the count rates from the side crystals are equal; this assures that essentially all elastically scattered deuterons strike the center crystal, so that their intensity can be measured with a single magnet setting. It also provides sufficient energy resolution, ($\sim 150 \text{ keV}$) so that there can be no contribution from inelastic scattering even to first excited states for any of the nuclei studied. The detector is covered with sufficient absorber to eliminate tritons, and neither protons nor alpha particles have sufficient magnetic rigidity to reach the detector. In a few cases at back angles, the elastic peak was too wide to be detected by the center crystal only, so that corrections were applied using the count rate in the side crystals.

The incident deuteron energy cannot be carefully



FIG. 1. Schematic diagram of the detector for the 15-MeV deuteron elastic angular distributions. Details of design and operation are explained in the text. PM-A, PM-B, and PM-C are photomultiplier tubes. The graph in the top part is the intensity distribution of elastically scattered deuterons across the crystals. By varying the analyzing magnetic field almost the entire elastic deuteron group could be made to fall on the center crystal as indicated in this figure.

TABLE I. $(\sigma/\sigma_R)_{e.m.}$ vs $\theta_{e.m.}$ for 15-MeV deuterons elastically scattered from several elements.

Al Ti Fe Ni ²⁹ Cu Ni ²⁹ Cu q_{em} $(e^{r}eh)_{em}$ θ_{em} $(e^{r}eh)_{em}$ θ_{em} $(e^{r}eh)_{em}$ θ_{em} $(e^{r}eh)_{em}$ 2^{11} 18' 0.920 12' 2' 0' 0.651 21' 55' 0.666 23' 10' 0.733 97' 20' 0.122 23' 11' 0.636 20' 36' 0.550 24' 3' 0' 0.497 23' 20' 0.415 25' 54' 0.47' 99' 49' 0.0540 25' 10' 0.452 21' 20' 416 27' 2' 0' 0' 41' 12' 13' 0.366 21' 35' 0.0321 33' 31' 0.037' 11' 10' 4048 30' 32' 0.4453 31' 10' 20' 11 20' 43' 0.275 29' 48' 0.332 33' 31' 0.037' 11' 10' 00' 4048 30' 32' 0' 0.453 41' 22' 0.073 33' 2' 3' 0.477 14' 23' 0.351 44' 6' 0' 0.0349 11' 10' 00' 00448 4'' 8' 0.490 45' 10' 0.470 35' 3' 0' 0' 32' 3' 3' 0' 0' 32' 3' 3' 3' 0.350 4'' 0' 0' 30' 3' 11' 0' 30' 00474 38'' 35' 0.550 46' 13' 0' 0' 0' 0' 47' 3' 11' 0' 0' 47' 3' 3'' 3' 0' 30' 0' 47' 3' 3'' 3'' 0' 30' 0' 47' 3'' 3'' 3'' 0' 30' 0' 4'' 3'' 0' 40''' 0' 4''' 4''					· · · · · · · · · · · · · · · · · · ·	
θ_{cm} $(\sigma'\sigma x)_{cm}$ θ_{cm} $(\sigma'\sigma x)_{cm}$ θ_{cm} $(\sigma'\sigma x)_{cm}$ θ_{cm} $(\sigma'\sigma x)_{cm}$ 21* 18' 0.20 19'''' 0.711 10'''' 17''''' 0.735 20''''''''' 0.738 9'''''''''' 0.734 22'''''''''''''''''''''''''''''''''''	Al	Ti	Fe		Ni ⁵⁸	Cu
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$	$\theta_{\rm e.m.}$ $(\sigma/\sigma_R)_{\rm e.m.}$	$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$	$\theta_{e.m.}$	$(\sigma/\sigma_R)_{\rm c.m.}$	$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$
$ \begin{array}{c} 12 & 10 & 0.300 \\ 24 & 50 & 0.260 \\ 24 & 50 & 0.49 & 0.480 \\ 25 & 50 & 0.260 & 24 & 51 \\ 25 & 50 & 0.271 & 0.076 & 27 & 0.076 \\ 25 & 50 & 0.28 & 0.372 & 37 & 0.077 & 10 \\ 25 & 50 & 0.28 & 0.372 & 31 & 0.37 & 31 & 0.076 & 12 & 91 & 0.056 \\ 31 & 27 & 0.21 & 0.28 & 0.28 & 0.332 & 31 & 0.33 & 0.352 & 100^{4} & 48 & 0.0498 & 30 & 55 & 0.465 \\ 34 & 31 & 0.294 & 32^{2} & 2.28 & 0.333 & 32^{2} & 22 & 0.332 & 33^{2} & 70 & .797 & 107^{2} & 10.084 & 30 & 55 & 0.465 \\ 37^{2} & 10 & 0.413 & 34^{2} & 58 & 0.377 & 34^{2} & 44^{2} & 34^{2} & 0.424 & 38^{6} & 40 & 0.501 & 112^{1} & 30 & 0.049 & 36^{6} & 10 & .502 \\ 39^{4} & 7 & 0.533 & 37^{2} & 33^{2} & 0.377 & 34^{2} & 0.472 & 38^{4} & 36^{2} & 11 & 0.511 & 114^{2} & 40 & 0.0948 & 41^{2} & 8 & 0.490 \\ 45^{7} & 20^{2} & 0.532 & 45^{2} & 16 & 0.476 & 45^{2} & 01^{2} & 0.384 & 43^{2} & 37 & 0.551 & 114^{2} & 40 & 0.0948 & 41^{2} & 8^{2} & 0.490 \\ 45^{7} & 20^{2} & 0.532 & 45^{2} & 16 & 0.476 & 45^{2} & 01^{2} & 0.484 & 51^{2} & 0.0561 & 112^{2} & 36 & 0.0055 & 46^{2} & 14^{2} & 0.435 \\ 50^{2} & 15^{2} & 0.079 & 47^{2} & 51^{2} & 0.422 & 47^{2} & 35^{2} & 0.360 & 49^{0} & 00 & 0.349 & 122^{2} & 04^{2} & 0.0048 & 48^{4} & 47 & 0.250 \\ 51^{2} & 51^{2} & 0.051 & 54^{2} & 14^{2} & 0.467 & 0.571 & 117^{2} & 08^{2} & 0.0055 & 54^{6} & 14^{2} & 0.448 \\ 55^{4} & 0.213 & 57^{2} & 0.018 & 120^{2} & 50 & 0.013 & 55^{2} & 0.118 \\ 65^{3} & 40^{2} & 0.351 & 120^{2} & 50 & 0.013 & 55^{2} & 0.118 \\ 65^{3} & 40^{2} & 0.351 & 115^{2} & 0.213 & 57^{2} & 10.218 & 115^{2} & 0.0131 & 55^{2} & 0.018 \\ 65^{4} & 52^{2} & 0.030 & 68^{1} & 52^{2} & 0.023 & 65^{2} & 70 & 0.222 & 141^{2} & 38^{2} & 0.051 & 11^{2} & 38^{2} & 0.026 \\ 65^{3} & 40^{2} & 0.261 & 67^{2} & 57^{2} & 0.221 & 141^{2} & 38 & 0.042 & 68^{2} & 37 & 0.284 \\ 65^{4} & 20^{2} & 0.171 & 0.255 & 0.271 & 0.258 & 0.278 & 0.278 & 0.278 \\ 77^{3} & 37^{3} & 0.58 & 67^{3} & 70 & 0.251 & 115^{2} & 57^{2} & 0.251 & 114^{2} & 38^{2} & 0.153 \\ 77^{3} & 32^{2} & 0.303 & 67^{2} & 7^{2} & 0.190 & 775^{2} & 7^{2} & 0.150 & 115^{2} & 7^{2} & 0.284 & $		109.07/ 0.771	109 17/ 0 725	2009 44/ 0 722	049 50/ 0 129	009 27/ 0 724
$ \begin{array}{c} 26 & 36 & 0 & 560 & 24^{+} 37^{+} 0 & 660 & 27^{+} 03^{+} 0 & 0481 & 22^{+} 84^{+} 0 & 0477 & 69^{+} 40^{+} 0 & 0550 & 28^{+} 9 & 0.481 \\ 31^{+} 33^{+} 0 & 0111 & 29^{+} 48^{+} 0 & 0753 & 29^{+} 38^{+} 33^{+} 31 & 031 & 0.552 & 104^{+} 48^{+} 0 & 0456 & 38^{+} 27^{+} 0 & 0451 \\ 34^{+} 31^{+} 0 & 0413 & 34^{+} 38^{+} 0 & 0733 & 20^{+} 38^{+} 33^{+} 37^{-} 0 & 377 & 107^{+} 17^{+} 0 & 0456 & 33^{+} 27^{-} 0 & 0451 \\ 33^{+} 31^{+} 0 & 0413 & 34^{+} 38^{+} 0 & 0733 & 0424 & 33^{+} 37^{-} 0 & 0510 & 112^{+} 31^{+} 0 & 0456 & 33^{+} 27^{-} 0 & 0454 \\ 42^{+} 23^{+} 0 & 0433 & 37^{+} 33^{+} 0 & 073 & 34^{+} 33^{+} 0 & 0424 & 36^{+} 11 & 0.479 & 109^{+} 45^{+} 0 & 0490 & 43^{+} 44^{+} 0 & 0494 \\ 45^{+} 30^{+} 0 & 054 & 04^{+} 0 & 0451 & 44^{+} 28^{+} 04^{+} 0 & 0454 & 44^{+} 8^{+} 64^{+} 0 & 0494 \\ 45^{+} 30^{+} 0 & 0552 & 45^{+} 16^{+} 0 & 0476 & 45^{+} 04^{+} 0 & 0481 & 44^{+} 28^{+} 0 & 0000 & 43^{+} 44^{+} 0 & 0424 \\ 47^{+} 30^{+} 0 & 0552 & 45^{+} 16^{+} 0 & 0476 & 45^{+} 04^{+} 0 & 0481 & 44^{+} 28^{+} 0 & 0000 & 43^{+} 44^{+} 0 & 0424 \\ 47^{+} 30^{+} 0 & 0522 & 54^{+} 13^{+} 0 & 0421 & 27^{+} 35^{+} 0 & 030 & 00^{+} 0 & 0349 & 122^{-} 04^{+} 0 & 00484 & 48^{+} 44^{+} 0 & 0345 \\ 52^{+} 51^{+} 0 & 0471 & 50^{+} 24^{+} 0 & 0342 & 52^{+} 41^{+} 0 & 0484 & 45^{+} 0^{+} 0 & 0218 & 127^{+} 0^{+} 0 & 00822 & 51^{+} 33^{+} 017 \\ 0.55^{+} 37^{+} 0 & 0.141 & 55^{+} 34^{+} 0 & 00^{+} 15^{+} 0 & 15^{+} 13^{+} 13^{+} 0 & 00448 & 45^{+} 0^{+} 0 & 0218 \\ 63^{+} 40^{+} 0 & 053 & 65^{+} 51^{+} 0 & 0.123 & 67^{+} 57^{+} 0 & 0.128 & 129^{+} 11^{+} 0 & 0449 & 01^{+} 38^{+} 0 & 0128 \\ 63^{+} 40^{+} 0 & 053 & 65^{+} 51^{+} 0 & 213 & 67^{+} 57^{+} 0 & 213 & 35^{+} 17^{+} 0 & 108 \\ 63^{+} 40^{+} 0 & 053 & 65^{+} 51^{+} 0 & 213 & 57^{+} 18^{+} 0 & 0188 & 129^{+} 57^{+} 0 & 226 & 0787 \\ 63^{+} 0 & 050 & 05^{+} 57^{+} 0 & 0342 & 52^{+} 10 & 214^{+} 14^{+} 0 & 0424 & 53^{+} 0 & 103 \\ 63^{+} 12^{+} 0 & 050 & 050 & 06^{+} 15^{+} 0 & 0214 & 157^{+} 57^{+} 0 & 226 & 0787 \\ 63^{+} 0 & 050 & 06^{+} 14^{+} 0 & 025 & 0787 \\ 63^{+} 0 & 050 & $	21° 18° 0.920 23° 57′ 0.700	$19^{\circ} 27^{\circ} 0.771$ 22° 03′ 0.665	19° 17' 0.735 21° 55' 0.686	$20^{\circ} 44^{\circ} 0.723$ $23^{\circ} 10^{\circ} 0.578$	94° 50° 0.138 07° 20′ 0.122	20° 37° 0.734 23° 11′ 0.680
$ \begin{array}{c} 29 - 12' & 0.416 & 27^{\circ} 10' & 0.465 & 27^{\circ} 03' & 0.415 & 28^{\circ} 20' & 0.386 & 102^{\circ} 10' & 0.0498 & 28^{\circ} 10' & 0.482 \\ 31^{\circ} 53' & 0.416 & 32^{\circ} 23' & 0.233 & 32^{\circ} 22' & 0.332 & 33^{\circ} 47' & 0.397 & 107^{\circ} 17' & 0.0498 & 30^{\circ} 23' & 0.454 \\ 37' 10' & 0.413 & 34' 85' & 0.377 & 34' 33' & 0.427 & 33' 31' & 0.472 & 38^{\circ} 44' & 0.506 & 112' 13 & 0.0747 & 38^{\circ} 35' & 0.528 \\ 32' 25' & 0.773 & 40'' 06'' & 0.469 & 39'' 53'' & 0.503 & 41'' 20'' & 0.511 & 114'' 40'' & 0.0948 & 44^{\circ} 41' & 0.442 \\ 45'' 02'' & 0.015 & 42'' 43'' & 0.497 & 42'' 28'' & 0.508 & 44'' 53'' & 0.507 & 117'' 08'' & 0.0948 & 44^{\circ} 41'' & 0.442 \\ 45'' 02'' & 0.052 & 45'' 10' & 0.476 & 45'' 01'' & 0.416 & 46'' 27'' & 0.426 & 119'' 36'' & 0.0955 & 44^{\circ} 41'' & 0.345 \\ 50'' 15'' & 0.679 & 47'' 51'' & 0.427 & 47'' 35'' & 0.300 & 49'' 00'' & 0.349 & 122'' 04'' & 0.0985 & 51'' 20'' & 0.195 \\ 52'' 51'' & 0.194 & 53'' & 0.342 & 52'' 41'' & 0.248 & 54'' 06'' & 0.181 & 129''' 10'' & 0.0822 & 33''' 53''' & 0.178 \\ 53'' 05'' & 0.159 & 55'' 10'' & 0.123 & 55'' 11'' & 0.185 & 129''' 21''' 0'''''''''''''''''''''''''''''$	25 57 0.199 26° 36′ 0.560	22 03 0.003 24° 37′ 0.407	21 33 0.080 23° 20′ 0.481	25° 54′ 0.477	97 20 0.122 00° 40′ 0.0764	25° 45′ 0 523
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	20° 12′ 0.416	27° 21′ 0.366	$20^{\circ} 23^{\circ} 0.101^{\circ}$ $27^{\circ} 03' 0.415^{\circ}$	28° 29 0.386	102° 19′ 0.0540	28° 19 0.482
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	31° 53′ 0.311	29° 48′ 0.275	29° 38′ 0.335	31° 03 0.352	104° 48′ 0.0498	30° 53 0.465
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	34° 31′ 0.294	32° 23′ 0.283	32° 22′ 0.332	33° 37 0.397	107° 17′ 0.0456	33° 27 0.454
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	37° 10′ 0.413	34° 58′ 0.377	34° 43′ 0.424	36° 11 0.479	109° 45′ 0.0449	36° 01 0.502
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	39° 47′ 0.583	37° 33′ 0.427	37° 31′ 0.472	38° 46′ 0.506	112° 13 0.0747	38° 35′ 0.528
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	42° 25′ 0.773	40° 08′ 0.469	39° 53′ 0.503	41° 20′ 0.531	114° 40′ 0.0948	41° 8′ 0.490
$ \begin{array}{c} 4' \ 3'' \ 0.582 \ 4'' \ 10' \ 0.4'' \ 4'' \ 10' \ 0.4'' \ 10' \ 10' \ 10' \ 10' \ 10' \ 0.0'' \ 0.0'' \ 0.0'' \ 0.2''' \ 0.0''' \ 0.2''''' \ 0.0'''''''''''''''''''''''''''''$	45° 02′ 0.915	42° 43′ 0.497	42° 28′ 0.508	43° 53′ 0.507	117° 08′ 0.0940	43° 41′ 0.442
$ \begin{array}{c} 32 & 51 \\ 32 & 51 \\ 32 & 51 \\ 34 & 31 \\ 35 & 32 \\ 35 & 37 \\ 0.314 \\ 32 & 52 \\ 35 & 37 \\ 0.314 \\ 32 & 52 \\ 58 & 32 \\ 0.33 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.33 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.33 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.33 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.33 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.33 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.35 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.35 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.35 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.35 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.35 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.35 \\ 35 & 31 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 35 & 32 \\ 0.31 \\ 0.31 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ $	47° 39' 0.852	45° 10' 0.470	45° 01' 0.451	40° 27' 0.420	119° 30° 0.0955	40° 14' 0.345
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	50° 15° 0.079 52° 51′ 0.471	47 51 0.427 50° 24′ 0.367	47 33 0.300 50° 07' 0.282	49 00 0.349 51° 33′ 0.260	122 04 0.0948	40 47 0.230 51° 20′ 0.100
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$52^{\circ} 37' = 0.314$	52° 59′ 0.342	52° 41′ 0.248	54° 06′ 0.218	127° 0′ 0.0822	53° 53′ 0.178
$ \begin{array}{c} 69\ 27' \ 0.165 \ 58^{\circ}\ 0.70 \ 318 \ 57'\ 47'\ 0.209 \ 59^{\circ}\ 11'\ 0.195 \ 131' 52'\ 0.0556 \ 58''\ 58''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 54''\ 0.246 \ 56''\ 0.246 \ 56''\ 0.246 \ 56''\ 0.246 \ 56''\ 0.246 \ 56''\ 0.246 \ 55''\ 0.246 \ 55''\ 0.246 \ 55''\ 0.246 \ 55'''\ 0.246 \ 55'''\ 0.246 \ 55'''\ 0.246 \ 55'''\ 0.246 \ 55'''\ 0.$	58° 02′ 0.193	55° 31′ 0.312	55° 13′ 0.197	56° 39′ 0.188	129° 25′ 0.0731	56° 26′ 0.184
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	60° 37′ 0.165	58° 05′ 0.318	57° 47′ 0.209	59° 11′ 0.195	131° 52′ 0.0556	58° 58′ 0.208
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	63° 12′ 0.229	60° 37′ 0.309	60° 15′ 0.213	61° 43′ 0.205	134° 19′ 0.0449	61° 30′ 0.246
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	65° 46′ 0.367	63° 11′ 0.295	62° 51′ 0.218	64° 16′ 0.218	136° 45′ 0.0531	63° 32′ 0.284
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	68° 20′ 0.521	65° 43′ 0.263	65° 23′ 0.222	66° 48′ 0.218	139° 11′ 0.0465	66° 34′ 0.260
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	70° 53′ 0.680	68° 15′ 0.220	67° 54′ 0.219	69° 20′ 0.225	141° 38 0.0432	68° 36′ 0.251
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	73° 26′ 0.803	70° 47′ 0.162	70° 27′ 0.199	71° 52′ 0.218		71° 38′ 0.242
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	75° 58' 0.848	73° 20° 0.121 75° 51′ 0.124	72° 59° 0.196	74° 24° 0.219		73° 39' 0.221 76° 40' 0.199
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	81°02′0 704	73 31 0.124 78° 23′ 0.130	73 30 0.192 78°01′ 0.195	70 55 0.220 70° 26′ 0.218		70 40 0.168 78° 41′ 0.162
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	83° 34′ 0.600	80° 53′ 0.176	80° 32′ 0.202	81° 57′ 0.210		81° 42′ 0.146
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	86° 04′ 0.467	83° 24′ 0.230	83° 03′ 0.206	84° 27′ 0.193		83° 42′ 0.135
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	88° 35′ 0.356	85° 54′ 0.284	85° 33′ 0.196	86° 58′ 0.170		86° 42′ 0.114
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	91° 05′ 0.265	88° 25′ 0.321	88° 03′ 0.180	89° 28′ 0.157		88° 43′ 0.113
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	93° 35′ 0.197	90° 55′ 0.331	90° 34′ 0.170	92°00′ 0.130		91° 43′ 0.100
LatLatLatImage for the form of the						
$0_{c.m.}$			7.	V	Nib	Ma
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Zn $\theta_{1} = (\sigma/\sigma_{R})_{1} = 1$	θ	Zr	Y	Nb $\theta_{rm} = (\sigma/\sigma_{R})_{rm}$	$Mo = (\sigma/\sigma p) = 0$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$Zn \\ \theta_{c.m.} (\sigma/\sigma_R)_{c.m.}$	θ _{c.m.}	$\operatorname{Zr}_{(\sigma/\sigma_R)_{c.m.}}$	$\begin{array}{c} Y\\ \theta_{\mathrm{c.m.}} (\sigma/\sigma_R)_{\mathrm{c.m.}} \end{array}$	Nb $\theta_{c.m.}$ $(\sigma/\sigma_R)_{c.m.}$	$\begin{array}{l} \text{Mo}\\ \theta_{\text{c.m.}} (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ Zn \theta_{c.m.} (\sigma/\sigma_R)_{c.m.} $ 20° 36′ 0.707	θ _{e.m.}	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160	$\begin{array}{c} Y\\ \theta_{c.m.} & (\sigma/\sigma_R)_{c.m.}\\ \hline 20^{\circ} 26' & 0.800 \end{array}$	Nb $\theta_{\text{o.m.}} (\sigma/\sigma_R)_{\text{c.m.}}$ 19° 46′ 0.851	Mo $\theta_{\text{c.m.}} (\sigma/\sigma_R)_{\text{c.m.}}$ 19° 57′ 0.926
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		θ _{c.m.} 20° 28′ 0.905 23° 01′ 0.840	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.}\\ \hline 20^{\circ} 26' & 0.800\\ 22^{\circ} 59' & 0.787 \end{array}$	Nb $\theta_{\text{c.m.}}$ $(\sigma/\sigma_R)_{\text{c.m.}}$ 19° 46′ 0.851 22° 18′ 0.825	$\begin{array}{c} \text{Mo} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ 19^{\circ} 57' & 0.926 \\ 22^{\circ} 30' & 0.855 \end{array}$
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		θ _{c.m.} 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.}\\ \hline 20^{\circ} 26' & 0.800\\ 22^{\circ} 59' & 0.787\\ 25^{\circ} 32' & 0.692 \end{array}$	$\begin{array}{c} \text{Nb} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 19^{\circ} 46' & 0.851 \\ 22^{\circ} 18' & 0.825 \\ 24^{\circ} 51' & 0.740 \end{array}$	$\begin{array}{c} \text{Mo} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 19^\circ 57' & 0.926 \\ 22^\circ 30' & 0.855 \\ 25^\circ 03' & 0.731 \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} & Zn \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 20^{\circ} 36' & 0.707 \\ 23^{\circ} 11' & 0.660 \\ 25^{\circ} 45' & 0.486 \\ 28^{\circ} 19 & 0.459 \end{array}$	θ _{c.m.} 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.}\\ \hline 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ \hline \end{array}$	$\begin{array}{c} \text{Nb} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 19^{\circ} 46' & 0.851 \\ 22^{\circ} 18' & 0.825 \\ 24^{\circ} 51' & 0.740 \\ 27^{\circ} 24' & 0.690 \end{array}$	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 19^\circ 57' & 0.926\\ 22^\circ 30' & 0.855\\ 25^\circ 03' & 0.731\\ 27^\circ 36' & 0.630 \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} & Zn \\ \theta_{c.m.} & (\sigma/\sigma_R)_{e.m.} \end{array}$ 20° 36′ 0.707 23° 11′ 0.660 25° 45′ 0.486 28° 19 0.459 30° 53 0.440	<i>θ</i> _{c.m.} 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$ 20° 26′ 0.800 22° 59′ 0.787 25° 32′ 0.692 28° 05′ 0.616 30° 38′ 0.551	Nb $\theta_{\text{c.m.}}$ $(\sigma/\sigma_R)_{\text{c.m.}}$ 19° 46′ 0.851 22° 18′ 0.825 24° 51′ 0.740 27° 24′ 0.690 29° 42′ 0.566	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 19^{\circ} 57' & 0.926\\ 22^{\circ} 30' & 0.855\\ 25^{\circ} 03' & 0.731\\ 27^{\circ} 36' & 0.630\\ 30^{\circ} 08' & 0.553 \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} Zn \\ \theta_{c.m.} & (\sigma/\sigma_R)_{c.m.} \\ \hline 20^{\circ} 36' & 0.707 \\ 23^{\circ} 11' & 0.660 \\ 25^{\circ} 45' & 0.486 \\ 28^{\circ} 19 & 0.459 \\ 30^{\circ} 53 & 0.440 \\ 33^{\circ} 27 & 0.423 \\ 36^{\circ} 54' & 0.457 \\ \hline \end{array} $	<i>θ</i> _{c.m.} 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 106° 35′ 0.047	$\begin{array}{c} Y\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}}\\ \hline 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 33^\circ 11' & 0.492\\ \hline \end{array}$	Nb $\theta_{\text{c.m.}}$ $(\sigma/\sigma_R)_{\text{c.m.}}$ 19° 46′ 0.851 22° 18′ 0.825 24° 51′ 0.740 27° 24′ 0.690 29° 42′ 0.566 32° 29′ 0.504	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 19^\circ 57' & 0.926\\ 22^\circ 30' & 0.855\\ 25^\circ 03' & 0.731\\ 27^\circ 36' & 0.630\\ 30^\circ 08' & 0.553\\ 32^\circ 41' & 0.462\\ 32^\circ 41' & 0.462 \end{array}$
43° 43° 43° 21° 0.355 116° 31° 0.099 43° 22° 0.321 42° 41° 0.378 42° 11° 0.350 46° 14° 0.275 45° 56° 0.344 118° 59° 0.321 42° 41° 0.378 42° 13° 30° 48° 47° 0.200 48° 28° 0.334 121° 27° 0.115 45° 51° 0.347 45° 23° 0.307 48° 47° 0.00 48° 28° 0.334 121° 27° 0.117 48° 26° 0.27° 47° 46° 0.331 47° 55° 0.286 51° 0.152 51° 0.348 123° 55° 0.111 50° 88° 0.257 50° 18° 0.334 50° 26° 0.287 56° 26° 0.175 53° 32° 0.360 128° 51° 0.366 52° 0.340 52° 83° 0.287 56° 26° 0.175 58° 35° 0.257 50° 0.340 55° 0.287 58° 0.250 61° 07° 0.296 133° 47° 0.352 57° 53° 0.229 56° <t< td=""><td>$\begin{array}{c} & Zn \\ \theta_{c.m.} & (\sigma/\sigma_R)_{c.m.} \end{array}$</td><td><i>θ</i>_{c.m.} 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 28° 10′ 0.427</td><td>Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 1111° 23′ 0.073</td><td>$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline 20^{\circ} 26' & 0.800\\ 22^{\circ} 59' & 0.787\\ 25^{\circ} 32' & 0.692\\ 28^{\circ} 05' & 0.616\\ 30^{\circ} 38' & 0.551\\ 33^{\circ} 11' & 0.492\\ 35^{\circ} 44' & 0.444\\ 28^{\circ} 17' & 0.417 \\ \hline \end{array}$</td><td>Nb $\theta_{\text{c.m.}}$ $(\sigma/\sigma_R)_{\text{c.m.}}$ 19° 46′ 0.851 22° 18′ 0.825 24° 51′ 0.740 27° 24′ 0.690 29° 42′ 0.566 32° 29′ 0.504 35° 03′ 0.452 27° 26′ 0.445</td><td>$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 19^\circ 57' & 0.926\\ 22^\circ 30' & 0.855\\ 25^\circ 03' & 0.731\\ 27^\circ 36' & 0.630\\ 30^\circ 08' & 0.553\\ 32^\circ 41' & 0.462\\ 35^\circ 14' & 0.435\\ 27^\circ 44' & 0.410 \end{array}$</td></t<>	$\begin{array}{c} & Zn \\ \theta_{c.m.} & (\sigma/\sigma_R)_{c.m.} \end{array}$	<i>θ</i> _{c.m.} 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 28° 10′ 0.427	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 1111° 23′ 0.073	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline 20^{\circ} 26' & 0.800\\ 22^{\circ} 59' & 0.787\\ 25^{\circ} 32' & 0.692\\ 28^{\circ} 05' & 0.616\\ 30^{\circ} 38' & 0.551\\ 33^{\circ} 11' & 0.492\\ 35^{\circ} 44' & 0.444\\ 28^{\circ} 17' & 0.417 \\ \hline \end{array}$	Nb $\theta_{\text{c.m.}}$ $(\sigma/\sigma_R)_{\text{c.m.}}$ 19° 46′ 0.851 22° 18′ 0.825 24° 51′ 0.740 27° 24′ 0.690 29° 42′ 0.566 32° 29′ 0.504 35° 03′ 0.452 27° 26′ 0.445	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 19^\circ 57' & 0.926\\ 22^\circ 30' & 0.855\\ 25^\circ 03' & 0.731\\ 27^\circ 36' & 0.630\\ 30^\circ 08' & 0.553\\ 32^\circ 41' & 0.462\\ 35^\circ 14' & 0.435\\ 27^\circ 44' & 0.410 \end{array}$
$46^{\circ} 14'$ 0.275 $45^{\circ} 56'$ 0.344 $118^{\circ} 59'$ 0.115 $45^{\circ} 54'$ 0.297 $45^{\circ} 13'$ 0.347 $45^{\circ} 23'$ 0.307 $48^{\circ} 47'$ 0.200 $48^{\circ} 28'$ 0.334 $121^{\circ} 27'$ 0.117 $48^{\circ} 26'$ 0.270 $47^{\circ} 46'$ 0.331 $47^{\circ} 55'$ 0.286 $51^{\circ} 20'$ 0.152 $51^{\circ} 0'$ 0.348 $123^{\circ} 55'$ 0.111 $50^{\circ} 58'$ 0.257 $50^{\circ} 18'$ 0.334 $50^{\circ} 26'$ 0.287 $53^{\circ} 53'$ 0.175 $53^{\circ} 32'$ 0.355 $126^{\circ} 23'$ 0.096 $53^{\circ} 30'$ 0.306 $52^{\circ} 50'$ 0.340 $52^{\circ} 58'$ 0.287 $56^{\circ} 26'$ 0.190 $56^{\circ} 04'$ 0.360 $128^{\circ} 51'$ 0.087 $56^{\circ} 02'$ 0.334 $55^{\circ} 22'$ 0.340 $55^{\circ} 30'$ 0.279 $58^{\circ} 58'$ 0.217 $58^{\circ} 35'$ 0.348 $131^{\circ} 19'$ 0.077 $58^{\circ} 33'$ 0.352 $57^{\circ} 54'$ 0.332 $58^{\circ} 02'$ 0.263 $51^{\circ} 0.250$ $61^{\circ} 07'$ 0.296 $133^{\circ} 47'$ 0.067 $61^{\circ} 05'$ 0.344 $60^{\circ} 25'$ 0.298 $60^{\circ} 33'$ 0.242 $63^{\circ} 32'$ 0.252 $63^{\circ} 39'$ 0.244 $136^{\circ} 15'$ 0.54 $63^{\circ} 36'$ 0.271 $62^{\circ} 57'$ 0.259 $63^{\circ} 04'$ 0.206 $66^{\circ} 34'$ 0.238 $66^{\circ} 10'$ 0.179 $138^{\circ} 43'$ 0.050 $66^{\circ} 07'$ 0.220 $65^{\circ} 29'$ 0.213 65	$\begin{array}{c} & Zn \\ \theta_{c.m.} & (\sigma/\sigma_R)_{e.m.} \end{array}$	$\theta_{\rm c.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404	Zr $(\sigma/\sigma_R)_{\text{c.m.}}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 35^\circ 44' & 0.444\\ 38^\circ 17' & 0.417\\ 40^\circ 49' & 0.350 \\ \hline \end{array}$	Nb $\theta_{\text{c.m.}}$ $(\sigma/\sigma_R)_{\text{c.m.}}$ 19° 46′ 0.851 22° 18′ 0.825 24° 51′ 0.740 27° 24′ 0.690 29° 42′ 0.566 32° 29′ 0.504 35° 03′ 0.452 37° 36′ 0.445 40° 08′ 0.401	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 19^\circ 57' & 0.926\\ 22^\circ 30' & 0.855\\ 25^\circ 03' & 0.731\\ 27^\circ 36' & 0.630\\ 30^\circ 08' & 0.553\\ 32^\circ 41' & 0.462\\ 35^\circ 14' & 0.435\\ 37^\circ 44' & 0.419\\ 40^\circ 18' & 0.382 \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} & Zn \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\theta_{\rm c.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355	Zr $(\sigma/\sigma_R)_{\text{c.m.}}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 35^\circ 44' & 0.444\\ 38^\circ 17' & 0.417\\ 40^\circ 49' & 0.350\\ 43^\circ 22' & 0.321 \\ \hline \end{array}$	$\begin{array}{c} \text{Nb}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 19^{\circ} 46' & 0.851\\ 22^{\circ} 18' & 0.825\\ 24^{\circ} 51' & 0.740\\ 27^{\circ} 24' & 0.690\\ 29^{\circ} 42' & 0.566\\ 32^{\circ} 29' & 0.504\\ 35^{\circ} 03' & 0.452\\ 37^{\circ} 36' & 0.445\\ 40^{\circ} 08' & 0.401\\ 42^{\circ} 41' & 0.378 \end{array}$	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} & Zn \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\theta_{\rm c.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344	Zr $(\sigma/\sigma_R)_{\text{c.m.}}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 35^\circ 44' & 0.444\\ 38^\circ 17' & 0.417\\ 40^\circ 49' & 0.350\\ 43^\circ 22' & 0.321\\ 45^\circ 54' & 0.297 \\ \hline \end{array}$	$\begin{array}{c} \text{Nb}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$ $\begin{array}{c} 19^{\circ} 46' & 0.851\\ 22^{\circ} 18' & 0.825\\ 24^{\circ} 51' & 0.740\\ 27^{\circ} 24' & 0.690\\ 29^{\circ} 42' & 0.566\\ 32^{\circ} 29' & 0.504\\ 35^{\circ} 03' & 0.452\\ 37^{\circ} 36' & 0.445\\ 40^{\circ} 08' & 0.401\\ 42^{\circ} 41' & 0.378\\ 45^{\circ} 13' & 0.347 \end{array}$	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} & Zn \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$	$\begin{array}{c ccccc} \theta_{\rm c.m.} \\ \hline & 20^\circ 28' & 0.905 \\ 23^\circ 01' & 0.840 \\ 25^\circ 34' & 0.696 \\ 28^\circ 07' & 0.621 \\ 30^\circ 40' & 0.562 \\ 33^\circ 16' & 0.536 \\ 35^\circ 46' & 0.461 \\ 38^\circ 19' & 0.437 \\ 40^\circ 51' & 0.404 \\ 43^\circ 24' & 0.355 \\ 45^\circ 56' & 0.344 \\ 48^\circ 28' & 0.334 \\ \end{array}$	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 35^\circ 44' & 0.444\\ 38^\circ 17' & 0.417\\ 40^\circ 49' & 0.350\\ 43^\circ 22' & 0.321\\ 45^\circ 54' & 0.297\\ 48^\circ 26' & 0.270 \\ \hline \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} & \text{Mo} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline 19^\circ 57' & 0.926 \\ 22^\circ 30' & 0.855 \\ 25^\circ 03' & 0.731 \\ 27^\circ 36' & 0.630 \\ 30^\circ 08' & 0.553 \\ 32^\circ 41' & 0.462 \\ 35^\circ 14' & 0.435 \\ 37^\circ 44' & 0.419 \\ 40^\circ 18' & 0.382 \\ 42^\circ 51' & 0.350 \\ 45^\circ 23' & 0.307 \\ 47^\circ 55' & 0.286 \\ \hline \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} & Zn \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} \theta_{\rm c.m.} \\ \hline 20^{\circ} 28' & 0.905 \\ 23^{\circ} 01' & 0.840 \\ 25^{\circ} 34' & 0.696 \\ 28^{\circ} 07' & 0.621 \\ 30^{\circ} 40' & 0.562 \\ 33^{\circ} 16' & 0.536 \\ 35^{\circ} 46' & 0.461 \\ 38^{\circ} 19' & 0.437 \\ 40^{\circ} 51' & 0.404 \\ 43^{\circ} 24' & 0.355 \\ 45^{\circ} 56' & 0.344 \\ 48^{\circ} 28' & 0.334 \\ 51^{\circ} 0' & 0.348 \\ \end{array}$	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 35^\circ 44' & 0.444\\ 38^\circ 17' & 0.417\\ 40^\circ 49' & 0.350\\ 43^\circ 22' & 0.321\\ 45^\circ 54' & 0.297\\ 48^\circ 26' & 0.270\\ 50^\circ 58' & 0.257 \\ \hline \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} & \text{Mo} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline 19^\circ 57' & 0.926 \\ 22^\circ 30' & 0.855 \\ 25^\circ 03' & 0.731 \\ 27^\circ 36' & 0.630 \\ 30^\circ 08' & 0.553 \\ 32^\circ 41' & 0.462 \\ 35^\circ 14' & 0.445 \\ 35^\circ 14' & 0.435 \\ 37^\circ 44' & 0.419 \\ 40^\circ 18' & 0.382 \\ 42^\circ 51' & 0.350 \\ 45^\circ 23' & 0.307 \\ 45^\circ 23' & 0.307 \\ 47^\circ 55' & 0.286 \\ 50^\circ 26' & 0.287 \\ \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} & Zn \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 35^\circ 44' & 0.444\\ 38^\circ 17' & 0.417\\ 40^\circ 49' & 0.350\\ 43^\circ 22' & 0.321\\ 45^\circ 54' & 0.297\\ 48^\circ 26' & 0.270\\ 50^\circ 58' & 0.257\\ 53^\circ 30' & 0.306 \\ \hline \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	Mo $θ_{o.m.}$ $(σ/σ_R)_{o.m.}$ 19° 57′ 0.926 22° 30′ 0.855 25° 03′ 0.731 27° 36′ 0.630 30° 08′ 0.553 32° 41′ 0.462 35° 14′ 0.435 37° 44′ 0.419 40° 18′ 0.382 42° 51′ 0.350 45° 23′ 0.307 47° 55′ 0.286 50° 26′ 0.287 52° 58′ 0.287
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355 56° 04′ 0.360	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.099 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 121° 27′ 0.275	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 35^\circ 44' & 0.444\\ 38^\circ 17' & 0.417\\ 40^\circ 49' & 0.350\\ 43^\circ 22' & 0.321\\ 45^\circ 54' & 0.297\\ 48^\circ 26' & 0.270\\ 50^\circ 58' & 0.257\\ 53^\circ 30' & 0.306\\ 56^\circ 02' & 0.334\\ ree 23' & 0.557\\ \hline \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} \text{Zn} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355 56° 04′ 0.360 58° 35′ 0.348 51° 0′ 0.256	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 131° 19′ 0.077 132° 247′ 0.57	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline \\ 20^{\circ} 26' & 0.800\\ 22^{\circ} 59' & 0.787\\ 25^{\circ} 32' & 0.692\\ 28^{\circ} 05' & 0.616\\ 30^{\circ} 38' & 0.551\\ 33^{\circ} 11' & 0.492\\ 35^{\circ} 44' & 0.444\\ 38^{\circ} 17' & 0.417\\ 40^{\circ} 49' & 0.350\\ 43^{\circ} 22' & 0.321\\ 45^{\circ} 54' & 0.297\\ 48^{\circ} 26' & 0.270\\ 50^{\circ} 58' & 0.257\\ 53^{\circ} 30' & 0.306\\ 56^{\circ} 02' & 0.334\\ 58^{\circ} 33' & 0.352\\ 61^{\circ} 05' & 2.44 \\ \hline \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} & Zn \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \end{array}$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355 56° 04′ 0.360 58° 35′ 0.348 61° 0′ 0.296 63° 30′ 0.244	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 131° 19′ 0.077 133° 47′ 0.067 136° 15′ 0.054	$\begin{array}{c c} & Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline \\ 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 35^\circ 44' & 0.444\\ 38^\circ 17' & 0.417\\ 40^\circ 49' & 0.350\\ 43^\circ 22' & 0.321\\ 45^\circ 54' & 0.297\\ 48^\circ 26' & 0.270\\ 50^\circ 58' & 0.257\\ 53^\circ 30' & 0.306\\ 56^\circ 02' & 0.334\\ 58^\circ 33' & 0.352\\ 61^\circ 05' & 0.344\\ 63^\circ 66' & 0.271\\ \hline \end{array}$	$\begin{array}{c} \text{Nb}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline 19^{\circ} 46' & 0.851\\ 22^{\circ} 18' & 0.825\\ 24^{\circ} 51' & 0.740\\ 27^{\circ} 24' & 0.690\\ 29^{\circ} 42' & 0.566\\ 32^{\circ} 29' & 0.504\\ 35^{\circ} 03' & 0.452\\ 37^{\circ} 36' & 0.445\\ 40^{\circ} 08' & 0.401\\ 42^{\circ} 41' & 0.378\\ 45^{\circ} 13' & 0.347\\ 47^{\circ} 46' & 0.331\\ 50^{\circ} 18' & 0.334\\ 52^{\circ} 50' & 0.340\\ 55^{\circ} 22' & 0.340\\ 55^{\circ} 22' & 0.340\\ 55^{\circ} 22' & 0.322\\ 60^{\circ} 25' & 0.250\\ \hline \end{array}$	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline 19^\circ 57' & 0.926\\ 22^\circ 30' & 0.855\\ 25^\circ 03' & 0.731\\ 27^\circ 36' & 0.630\\ 30^\circ 08' & 0.553\\ 32^\circ 41' & 0.462\\ 35^\circ 14' & 0.442\\ 35^\circ 14' & 0.445\\ 37^\circ 44' & 0.419\\ 40^\circ 18' & 0.382\\ 42^\circ 51' & 0.350\\ 45^\circ 23' & 0.307\\ 47^\circ 55' & 0.286\\ 50^\circ 26' & 0.287\\ 55^\circ 30' & 0.279\\ 55^\circ 30' & 0.279\\ 58^\circ 02' & 0.263\\ 60^\circ 33' & 0.242\\ 63^\circ 04' & 0.206 \\ \hline \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} \mbox{Zn} \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355 56° 04′ 0.360 58° 35′ 0.348 61° 07′ 0.296 63° 39′ 0.244 66° 10′ 0 179	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 131° 19′ 0.077 133° 47′ 0.054 136° 15′ 0.054 138° 43′ 0.050	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array} \\ \hline \begin{array}{c} 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 35^\circ 44' & 0.444\\ 38^\circ 17' & 0.417\\ 40^\circ 49' & 0.350\\ 43^\circ 22' & 0.321\\ 45^\circ 54' & 0.297\\ 48^\circ 26' & 0.270\\ 50^\circ 58' & 0.257\\ 53^\circ 30' & 0.306\\ 56^\circ 02' & 0.334\\ 58^\circ 33' & 0.352\\ 61^\circ 05' & 0.271\\ 66^\circ 07' & 0.220 \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline 19^\circ 57' & 0.926\\ 22^\circ 30' & 0.855\\ 25^\circ 03' & 0.731\\ 27^\circ 36' & 0.630\\ 30^\circ 08' & 0.553\\ 32^\circ 41' & 0.462\\ 35^\circ 14' & 0.445\\ 35^\circ 14' & 0.445\\ 37^\circ 44' & 0.419\\ 40^\circ 18' & 0.382\\ 42^\circ 51' & 0.350\\ 45^\circ 23' & 0.307\\ 47^\circ 55' & 0.286\\ 50^\circ 26' & 0.287\\ 55^\circ 30' & 0.279\\ 58^\circ 02' & 0.263\\ 60^\circ 33' & 0.242\\ 63^\circ 04' & 0.206\\ 65^\circ 35' & 0 172 \\ \hline \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} \mbox{Zn} \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355 56° 04′ 0.360 58° 35′ 0.348 61° 07′ 0.296 63° 39′ 0.244 66° 10′ 0.179 68° 42′ 0.124	Zr $(\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 131° 19′ 0.077 133° 47′ 0.067 136° 15′ 0.054 138° 43′ 0.050 141° 10′ 0.049	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array} \\ \hline \begin{array}{c} 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 35^\circ 44' & 0.444\\ 38^\circ 17' & 0.417\\ 40^\circ 49' & 0.350\\ 43^\circ 22' & 0.321\\ 45^\circ 54' & 0.297\\ 48^\circ 26' & 0.270\\ 50^\circ 58' & 0.257\\ 53^\circ 30' & 0.306\\ 56^\circ 02' & 0.334\\ 58^\circ 33' & 0.352\\ 61^\circ 05' & 0.221\\ 66^\circ 07' & 0.220\\ 68^\circ 39' & 0.167 \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} & \text{Mo} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline 19^\circ 57' & 0.926 \\ 22^\circ 30' & 0.855 \\ 25^\circ 03' & 0.731 \\ 27^\circ 36' & 0.630 \\ 30^\circ 08' & 0.553 \\ 32^\circ 41' & 0.462 \\ 35^\circ 14' & 0.445 \\ 35^\circ 14' & 0.445 \\ 35^\circ 14' & 0.445 \\ 37^\circ 44' & 0.419 \\ 40^\circ 18' & 0.382 \\ 42^\circ 51' & 0.350 \\ 45^\circ 23' & 0.307 \\ 47^\circ 55' & 0.286 \\ 50^\circ 26' & 0.287 \\ 55^\circ 30' & 0.279 \\ 58^\circ 02' & 0.263 \\ 60^\circ 33' & 0.242 \\ 63^\circ 04' & 0.206 \\ 65^\circ 35' & 0.172 \\ 68^\circ 07' & 0.146 \\ \hline \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} {\rm Zn} \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm e.m.} \end{array}$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355 56° 04′ 0.360 58° 35′ 0.348 61° 07′ 0.296 63° 39′ 0.244 66° 10′ 0.179 68° 42′ 0.124 71° 13′ 0.103	$Zr \\ (\sigma/\sigma_R)_{c.m.} $ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 131° 19′ 0.077 133° 47′ 0.067 136° 15′ 0.054 138° 43′ 0.050 141° 10′ 0.049	$\begin{array}{c c} & Y \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline \\ 20^\circ 26' & 0.800 \\ 22^\circ 59' & 0.787 \\ 25^\circ 32' & 0.692 \\ 28^\circ 05' & 0.616 \\ 30^\circ 38' & 0.551 \\ 33^\circ 11' & 0.492 \\ 35^\circ 44' & 0.444 \\ 38^\circ 17' & 0.417 \\ 40^\circ 49' & 0.350 \\ 43^\circ 22' & 0.321 \\ 45^\circ 54' & 0.297 \\ 48^\circ 26' & 0.270 \\ 50^\circ 58' & 0.257 \\ 53^\circ 30' & 0.306 \\ 56^\circ 02' & 0.334 \\ 58^\circ 33' & 0.352 \\ 61^\circ 05' & 0.220 \\ 68^\circ 39' & 0.167 \\ 71^\circ 11' & 0.125 \\ \hline \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} & \text{Mo} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline 19^\circ 57' & 0.926 \\ 22^\circ 30' & 0.855 \\ 25^\circ 03' & 0.731 \\ 27^\circ 36' & 0.630 \\ 30^\circ 08' & 0.553 \\ 32^\circ 41' & 0.462 \\ 35^\circ 14' & 0.445 \\ 35^\circ 14' & 0.445 \\ 35^\circ 14' & 0.445 \\ 37^\circ 44' & 0.419 \\ 40^\circ 18' & 0.382 \\ 42^\circ 51' & 0.350 \\ 45^\circ 23' & 0.307 \\ 47^\circ 55' & 0.286 \\ 50^\circ 26' & 0.287 \\ 55^\circ 30' & 0.279 \\ 58^\circ 02' & 0.263 \\ 60^\circ 33' & 0.242 \\ 63^\circ 04' & 0.206 \\ 65^\circ 35' & 0.172 \\ 68^\circ 07' & 0.146 \\ 70^\circ 38' & 0.132 \\ \hline \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} {\rm Zn} \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} \theta_{\rm e.m.} \\ \hline \\ 20^{\circ} 28' & 0.905 \\ 23^{\circ} 01' & 0.840 \\ 25^{\circ} 34' & 0.696 \\ 28^{\circ} 07' & 0.621 \\ 30^{\circ} 40' & 0.562 \\ 33^{\circ} 16' & 0.536 \\ 35^{\circ} 46' & 0.461 \\ 38^{\circ} 19' & 0.437 \\ 40^{\circ} 51' & 0.404 \\ 43^{\circ} 24' & 0.355 \\ 45^{\circ} 56' & 0.344 \\ 48^{\circ} 28' & 0.334 \\ 51^{\circ} 0' & 0.348 \\ 53^{\circ} 32' & 0.355 \\ 56^{\circ} 04' & 0.360 \\ 58^{\circ} 35' & 0.348 \\ 61^{\circ} 07' & 0.296 \\ 63^{\circ} 39' & 0.244 \\ 66^{\circ} 10' & 0.179 \\ 68^{\circ} 42' & 0.124 \\ 71^{\circ} 13' & 0.103 \\ 73^{\circ} 44' & 0.105 \\ \hline \end{array}$	$Zr \\ (\sigma/\sigma_R)_{c.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 131° 19′ 0.077 133° 47′ 0.067 136° 15′ 0.054 138° 43′ 0.050 141° 10′ 0.049	$\begin{array}{c c} & Y \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline \\ 20^\circ 26' & 0.800 \\ 22^\circ 59' & 0.787 \\ 25^\circ 32' & 0.692 \\ 28^\circ 05' & 0.616 \\ 30^\circ 38' & 0.551 \\ 33^\circ 11' & 0.492 \\ 35^\circ 44' & 0.444 \\ 38^\circ 17' & 0.417 \\ 40^\circ 49' & 0.350 \\ 43^\circ 22' & 0.321 \\ 45^\circ 54' & 0.297 \\ 48^\circ 26' & 0.270 \\ 50^\circ 58' & 0.257 \\ 53^\circ 30' & 0.306 \\ 56^\circ 02' & 0.334 \\ 58^\circ 33' & 0.352 \\ 61^\circ 05' & 0.220 \\ 68^\circ 39' & 0.167 \\ 71^\circ 11' & 0.125 \\ 73^\circ 41' & 0.095 \\ \hline \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} & \text{Mo} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline 19^\circ 57' & 0.926 \\ 22^\circ 30' & 0.855 \\ 25^\circ 03' & 0.731 \\ 27^\circ 36' & 0.630 \\ 30^\circ 08' & 0.553 \\ 32^\circ 41' & 0.462 \\ 35^\circ 14' & 0.445 \\ 35^\circ 14' & 0.445 \\ 35^\circ 14' & 0.445 \\ 37^\circ 44' & 0.419 \\ 40^\circ 18' & 0.382 \\ 42^\circ 51' & 0.350 \\ 45^\circ 23' & 0.307 \\ 47^\circ 55' & 0.286 \\ 50^\circ 26' & 0.287 \\ 55^\circ 30' & 0.279 \\ 58^\circ 02' & 0.263 \\ 60^\circ 33' & 0.242 \\ 63^\circ 04' & 0.206 \\ 65^\circ 35' & 0.172 \\ 68^\circ 07' & 0.146 \\ 70^\circ 38' & 0.132 \\ 73^\circ 09' & 0.134 \\ \hline \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} {\rm Zn} \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355 56° 04′ 0.360 58° 35′ 0.348 61° 07′ 0.296 63° 39′ 0.244 66° 10′ 0.179 68° 42′ 0.124 71° 13′ 0.103 73° 44′ 0.105 76° 15′ 0.123	$Zr \\ (\sigma/\sigma_R)_{e.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 131° 19′ 0.077 133° 47′ 0.067 136° 15′ 0.054 138° 43′ 0.050 141° 10′ 0.049	$\begin{array}{c} Y\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline \\ 20^\circ 26' & 0.800\\ 22^\circ 59' & 0.787\\ 25^\circ 32' & 0.692\\ 28^\circ 05' & 0.616\\ 30^\circ 38' & 0.551\\ 33^\circ 11' & 0.492\\ 35^\circ 44' & 0.444\\ 38^\circ 17' & 0.417\\ 40^\circ 49' & 0.350\\ 43^\circ 22' & 0.321\\ 45^\circ 54' & 0.297\\ 48^\circ 26' & 0.270\\ 50^\circ 58' & 0.257\\ 53^\circ 30' & 0.306\\ 56^\circ 02' & 0.334\\ 58^\circ 33' & 0.352\\ 61^\circ 05' & 0.344\\ 63^\circ 36' & 0.271\\ 66^\circ 07' & 0.220\\ 68^\circ 39' & 0.167\\ 71^\circ 11' & 0.125\\ 73^\circ 41' & 0.095\\ 76^\circ 12' & 0.101\\ \hline \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} & \text{Mo} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline 19^\circ 57' & 0.926 \\ 22^\circ 30' & 0.855 \\ 25^\circ 03' & 0.731 \\ 27^\circ 36' & 0.630 \\ 30^\circ 08' & 0.553 \\ 32^\circ 41' & 0.462 \\ 35^\circ 14' & 0.445 \\ 35^\circ 14' & 0.445 \\ 35^\circ 14' & 0.435 \\ 37^\circ 44' & 0.419 \\ 40^\circ 18' & 0.382 \\ 42^\circ 51' & 0.350 \\ 45^\circ 23' & 0.307 \\ 47^\circ 55' & 0.286 \\ 50^\circ 26' & 0.287 \\ 52^\circ 58' & 0.287 \\ 55^\circ 30' & 0.279 \\ 58^\circ 02' & 0.263 \\ 60^\circ 33' & 0.242 \\ 63^\circ 04' & 0.206 \\ 65^\circ 35' & 0.172 \\ 68^\circ 07' & 0.134 \\ 75^\circ 39' & 0.130 \\ \hline \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} & Zn \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline \\ 20^{\circ} 36' & 0.707 \\ 23^{\circ} 11' & 0.660 \\ 25^{\circ} 45' & 0.486 \\ 28^{\circ} 19 & 0.459 \\ 30^{\circ} 53 & 0.440 \\ 33^{\circ} 27 & 0.423 \\ 36^{\circ} 01' & 0.455 \\ 38^{\circ} 35' & 0.466 \\ 41^{\circ} 8' & 0.435 \\ 43^{\circ} 41' & 0.360 \\ 46^{\circ} 14' & 0.275 \\ 48^{\circ} 47' & 0.200 \\ 51^{\circ} 20' & 0.152 \\ 53^{\circ} 53' & 0.175 \\ 55^{\circ} 26' & 0.190 \\ 58^{\circ} 58' & 0.217 \\ 61^{\circ} 30' & 0.252 \\ 66^{\circ} 34' & 0.238 \\ 68^{\circ} 36' & 0.238 \\ 71^{\circ} 38' & 0.206 \\ 73^{\circ} 39' & 0.187 \\ 76^{\circ} 40' & 0.154 \\ 78^{\circ} 41' & 0.133 \\ 78^{\circ} 41' & 0.154 \\ 78^$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355 56° 04′ 0.360 58° 35′ 0.348 61° 07′ 0.296 63° 39′ 0.244 66° 10′ 0.179 68° 42′ 0.124 71° 13′ 0.103 73° 44′ 0.105 76° 15′ 0.123 78° 46′ 0.450	Zr $(\sigma/\sigma_R)_{e.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 131° 19′ 0.077 133° 47′ 0.067 136° 15′ 0.054 138° 43′ 0.050 141° 10′ 0.049	$\begin{array}{c c} & Y \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline \\ 20^\circ 26' & 0.800 \\ 22^\circ 59' & 0.787 \\ 25^\circ 32' & 0.692 \\ 28^\circ 05' & 0.616 \\ 30^\circ 38' & 0.551 \\ 33^\circ 11' & 0.492 \\ 35^\circ 44' & 0.444 \\ 38^\circ 17' & 0.417 \\ 40^\circ 49' & 0.350 \\ 43^\circ 22' & 0.321 \\ 45^\circ 54' & 0.297 \\ 48^\circ 26' & 0.270 \\ 50^\circ 58' & 0.257 \\ 53^\circ 30' & 0.306 \\ 56^\circ 02' & 0.334 \\ 58^\circ 33' & 0.352 \\ 61^\circ 05' & 0.344 \\ 63^\circ 36' & 0.271 \\ 66^\circ 07' & 0.220 \\ 68^\circ 39' & 0.167 \\ 71^\circ 11' & 0.125 \\ 73^\circ 41' & 0.095 \\ 76^\circ 12' & 0.101 \\ 78^\circ 43' & 0.124 \\ \hline \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	Mo $θ_{o.m.}$ $(σ/σ_R)_{o.m.}$ 19° 57′ 0.926 22° 30′ 0.855 25° 03′ 0.731 27° 36′ 0.630 30° 08′ 0.553 32° 41′ 0.462 35° 14′ 0.435 37° 44′ 0.419 40° 18′ 0.382 42° 51′ 0.350 45° 23′ 0.307 47° 55′ 0.286 50° 26′ 0.287 52° 58′ 0.287 55° 30′ 0.279 58° 02′ 0.263 60° 33′ 0.242 63° 04′ 0.206 65° 35′ 0.132 73° 09′ 0.134 75° 39′ 0.130 78° 10′ 0.154
80 42 0.105 60 10 0.221 80 14 0.210 85 54 0.210 85 41 0.105 88° 43' 0.097 88° 52' 0.203 88° 45' 0.216 88° 0.206 88° 11' 0.154 91° 43' 0.089 91° 17' 0.189 91° 15' 0.204 90° 35' 0.190 90° 41' 0.148	$\begin{array}{c} & Zn \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline \\ 20^{\circ} 36' & 0.707 \\ 23^{\circ} 11' & 0.660 \\ 25^{\circ} 45' & 0.486 \\ 28^{\circ} 19 & 0.459 \\ 30^{\circ} 53 & 0.440 \\ 33^{\circ} 27 & 0.423 \\ 36^{\circ} 01' & 0.455 \\ 38^{\circ} 35' & 0.466 \\ 41^{\circ} 8' & 0.435 \\ 43^{\circ} 41' & 0.360 \\ 46^{\circ} 14' & 0.275 \\ 48^{\circ} 47' & 0.200 \\ 51^{\circ} 20' & 0.152 \\ 53^{\circ} 53' & 0.175 \\ 56^{\circ} 26' & 0.190 \\ 58^{\circ} 58' & 0.217 \\ 61^{\circ} 30' & 0.250 \\ 63^{\circ} 32' & 0.252 \\ 66^{\circ} 34' & 0.238 \\ 71^{\circ} 38' & 0.206 \\ 73^{\circ} 39' & 0.187 \\ 76^{\circ} 40' & 0.154 \\ 78^{\circ} 41' & 0.133 \\ 81^{\circ} 42' & 0.122 \\ 828' 44' & 0.122 \\ \end{array}$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355 55° 04′ 0.360 58° 35′ 0.348 61° 07′ 0.296 63° 39′ 0.244 66° 10′ 0.179 68° 42′ 0.124 71° 13′ 0.103 73° 44′ 0.105 76° 15′ 0.123 78° 46′ 0.50 81° 16′ 0.191	Zr $(\sigma/\sigma_R)_{e.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 131° 19′ 0.077 133° 47′ 0.067 136° 15′ 0.054 138° 43′ 0.050 141° 10′ 0.049	$\begin{array}{c c} & Y \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline \\ 20^{\circ} 26' & 0.800 \\ 22^{\circ} 59' & 0.787 \\ 25^{\circ} 32' & 0.692 \\ 28^{\circ} 05' & 0.616 \\ 30^{\circ} 38' & 0.551 \\ 33^{\circ} 11' & 0.492 \\ 35^{\circ} 44' & 0.444 \\ 38^{\circ} 17' & 0.417 \\ 40^{\circ} 49' & 0.350 \\ 43^{\circ} 22' & 0.321 \\ 45^{\circ} 54' & 0.297 \\ 48^{\circ} 26' & 0.270 \\ 50^{\circ} 58' & 0.257 \\ 53^{\circ} 30' & 0.306 \\ 56^{\circ} 02' & 0.334 \\ 58^{\circ} 33' & 0.352 \\ 61^{\circ} 05' & 0.344 \\ 63^{\circ} 36' & 0.271 \\ 66^{\circ} 07' & 0.220 \\ 68^{\circ} 39' & 0.167 \\ 71^{\circ} 11' & 0.125 \\ 73^{\circ} 41' & 0.095 \\ 76^{\circ} 12' & 0.101 \\ 78^{\circ} 43' & 0.124 \\ 81^{\circ} 14' & 0.143 \\ 82^{\circ} 44' & 252 \\ \hline \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} \text{Mo}\\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline 19^\circ 57' & 0.926\\ 22^\circ 30' & 0.855\\ 25^\circ 03' & 0.731\\ 27^\circ 36' & 0.630\\ 30^\circ 08' & 0.553\\ 32^\circ 41' & 0.462\\ 35^\circ 14' & 0.445\\ 35^\circ 14' & 0.445\\ 35^\circ 14' & 0.435\\ 37^\circ 44' & 0.419\\ 40^\circ 18' & 0.382\\ 42^\circ 51' & 0.350\\ 45^\circ 23' & 0.307\\ 47^\circ 55' & 0.286\\ 50^\circ 24' & 0.287\\ 55^\circ 30' & 0.279\\ 55^\circ 30' & 0.279\\ 58^\circ 02' & 0.263\\ 60^\circ 33' & 0.242\\ 63^\circ 04' & 0.206\\ 65^\circ 35' & 0.172\\ 68^\circ 07' & 0.146\\ 70^\circ 38' & 0.132\\ 73^\circ 09' & 0.134\\ 75^\circ 39' & 0.130\\ 78^\circ 10' & 0.154\\ 80^\circ 40' & 0.165\\ \end{array}$
91° 43′ 0.089 91° 17′ 0.189 91° 15′ 0.204 90° 35′ 0.190 90° 41′ 0.148	$\begin{array}{c} & Zn \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline \\ 20^{\circ} 36' & 0.707 \\ 23^{\circ} 11' & 0.660 \\ 25^{\circ} 45' & 0.486 \\ 28^{\circ} 19 & 0.459 \\ 30^{\circ} 53 & 0.440 \\ 33^{\circ} 27 & 0.423 \\ 36^{\circ} 01' & 0.455 \\ 38^{\circ} 35' & 0.466 \\ 41^{\circ} 8' & 0.435 \\ 43^{\circ} 41' & 0.360 \\ 46^{\circ} 14' & 0.275 \\ 48^{\circ} 47' & 0.200 \\ 51^{\circ} 20' & 0.152 \\ 53^{\circ} 53' & 0.175 \\ 56^{\circ} 26' & 0.190 \\ 58^{\circ} 58' & 0.217 \\ 61^{\circ} 30' & 0.250 \\ 63^{\circ} 32' & 0.252 \\ 66^{\circ} 34' & 0.238 \\ 68^{\circ} 36' & 0.238 \\ 71^{\circ} 38' & 0.206 \\ 73^{\circ} 39' & 0.187 \\ 76^{\circ} 40' & 0.154 \\ 78^{\circ} 41' & 0.133 \\ 81^{\circ} 42' & 0.102 \\ 86^{\circ} 41' & 0.105 \\ \hline \end{array}$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355 55° 04′ 0.360 58° 35′ 0.348 61° 07′ 0.296 63° 39′ 0.244 66° 10′ 0.179 68° 42′ 0.124 71° 13′ 0.103 73° 44′ 0.105 76° 15′ 0.123 78° 46′ 0.150 81° 16′ 0.221	Zr $(\sigma/\sigma_R)_{e.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 131° 19′ 0.077 133° 47′ 0.067 136° 15′ 0.054 138° 43′ 0.050 141° 10′ 0.049	Y $\theta_{o.m.}$ $(\sigma/\sigma_R)_{o.m.}$ 20° 26' 0.800 22° 59' 0.787 25° 32' 0.692 28° 05' 0.616 30° 38' 0.551 33° 11' 0.492 35° 44' 0.444 38° 17' 0.417 40° 49' 0.350 43° 22' 0.221 45° 54' 0.297 48° 26' 0.270 50° 58' 0.257 53° 30' 0.306 56° 02' 0.334 58° 33' 0.352 61° 05' 0.344 63° 36' 0.271 66° 07' 0.220 68° 39' 0.167 71° 11' 0.125 73° 41' 0.095 76° 12' 0.101 78° 43' 0.124 81° 14' 0.143 83° 44' 0.193 86° 14' 0.216	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} \text{Mo}\\ \theta_{\text{e.m.}} & (\sigma/\sigma_R)_{\text{e.m.}} \\ \hline \\ 19^{\circ} 57' & 0.926\\ 22^{\circ} 30' & 0.855\\ 25^{\circ} 03' & 0.731\\ 27^{\circ} 36' & 0.630\\ 30^{\circ} 08' & 0.553\\ 32^{\circ} 41' & 0.462\\ 35^{\circ} 14' & 0.445\\ 35^{\circ} 14' & 0.445\\ 35^{\circ} 14' & 0.435\\ 37^{\circ} 44' & 0.419\\ 40^{\circ} 18' & 0.382\\ 42^{\circ} 51' & 0.350\\ 45^{\circ} 23' & 0.307\\ 47^{\circ} 55' & 0.286\\ 50^{\circ} 26' & 0.287\\ 55^{\circ} 30' & 0.279\\ 58^{\circ} 02' & 0.263\\ 60^{\circ} 33' & 0.242\\ 63^{\circ} 04' & 0.206\\ 65^{\circ} 35' & 0.172\\ 68^{\circ} 07' & 0.134\\ 70^{\circ} 38' & 0.132\\ 73^{\circ} 09' & 0.134\\ 75^{\circ} 39' & 0.130\\ 78^{\circ} 10' & 0.154\\ 80^{\circ} 40' & 0.165\\ 83^{\circ} 11' & 0.169\\ \end{array}$
	$\begin{array}{c} & Zn \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline \\ 20^{\circ} 36' & 0.707 \\ 23^{\circ} 11' & 0.660 \\ 25^{\circ} 45' & 0.486 \\ 28^{\circ} 19 & 0.459 \\ 30^{\circ} 53 & 0.440 \\ 33^{\circ} 27 & 0.423 \\ 36^{\circ} 01' & 0.455 \\ 38^{\circ} 35' & 0.466 \\ 41^{\circ} 8' & 0.435 \\ 43^{\circ} 41' & 0.360 \\ 46^{\circ} 14' & 0.275 \\ 48^{\circ} 47' & 0.200 \\ 51^{\circ} 20' & 0.152 \\ 53^{\circ} 53' & 0.175 \\ 56^{\circ} 26' & 0.190 \\ 58^{\circ} 58' & 0.217 \\ 61^{\circ} 30' & 0.250 \\ 63^{\circ} 32' & 0.252 \\ 66^{\circ} 34' & 0.238 \\ 68^{\circ} 36' & 0.238 \\ 71^{\circ} 38' & 0.206 \\ 73^{\circ} 39' & 0.187 \\ 76^{\circ} 40' & 0.154 \\ 78^{\circ} 41' & 0.133 \\ 81^{\circ} 42' & 0.102 \\ 86^{\circ} 42' & 0.105 \\ 88^{\circ} 43' & 0.007 \\ \end{array}$	$\theta_{e.m.}$ 20° 28′ 0.905 23° 01′ 0.840 25° 34′ 0.696 28° 07′ 0.621 30° 40′ 0.562 33° 16′ 0.536 35° 46′ 0.461 38° 19′ 0.437 40° 51′ 0.404 43° 24′ 0.355 45° 56′ 0.344 48° 28′ 0.334 51° 0′ 0.348 53° 32′ 0.355 56° 04′ 0.360 58° 35′ 0.348 61° 07′ 0.296 63° 39′ 0.244 66° 10′ 0.179 68° 42′ 0.123 78° 46′ 0.150 81° 16′ 0.191 83° 47′ 0.210 86° 16′ 0.221 88° 52′ 0.203	Zr $(\sigma/\sigma_R)_{e.m.}$ 94° 7′ 0.160 96° 36′ 0.149 99° 6′ 0.098 101° 36′ 0.070 104° 06′ 0.058 106° 35′ 0.047 109° 04′ 0.057 111° 33′ 0.073 114° 02′ 0.098 116° 31′ 0.099 118° 59′ 0.115 121° 27′ 0.117 123° 55′ 0.111 126° 23′ 0.096 128° 51′ 0.087 131° 19′ 0.077 133° 47′ 0.067 136° 15′ 0.054 138° 43′ 0.050 141° 10′ 0.049	$\begin{array}{c c} & Y \\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \\ \hline \\ 20^\circ 26' & 0.800 \\ 22^\circ 59' & 0.787 \\ 25^\circ 32' & 0.692 \\ 28^\circ 05' & 0.616 \\ 30^\circ 38' & 0.551 \\ 33^\circ 11' & 0.492 \\ 35^\circ 44' & 0.444 \\ 38^\circ 17' & 0.417 \\ 40^\circ 49' & 0.350 \\ 43^\circ 22' & 0.321 \\ 45^\circ 54' & 0.297 \\ 48^\circ 26' & 0.270 \\ 50^\circ 58' & 0.257 \\ 53^\circ 30' & 0.306 \\ 56^\circ 02' & 0.334 \\ 58^\circ 33' & 0.352 \\ 61^\circ 05' & 0.344 \\ 63^\circ 36' & 0.271 \\ 66^\circ 07' & 0.220 \\ 68^\circ 39' & 0.167 \\ 71^\circ 11' & 0.125 \\ 73^\circ 41' & 0.095 \\ 76^\circ 12' & 0.101 \\ 78^\circ 43' & 0.124 \\ 81^\circ 14' & 0.143 \\ 83^\circ 44' & 0.198 \\ 86^\circ 14' & 0.216 \\ 88^\circ 45' & 0.216 \\ \end{array}$	$\begin{array}{c} \mbox{Nb}\\ \theta_{\rm c.m.} & (\sigma/\sigma_R)_{\rm c.m.} \end{array}$	$\begin{array}{c} & \text{Mo} \\ \theta_{\text{c.m.}} & (\sigma/\sigma_R)_{\text{c.m.}} \\ \hline 19^\circ 57' & 0.926 \\ 22^\circ 30' & 0.855 \\ 25^\circ 03' & 0.731 \\ 27^\circ 36' & 0.630 \\ 30^\circ 08' & 0.553 \\ 32^\circ 41' & 0.462 \\ 35^\circ 14' & 0.445 \\ 37^\circ 44' & 0.419 \\ 40^\circ 18' & 0.382 \\ 42^\circ 51' & 0.350 \\ 45^\circ 23' & 0.307 \\ 45^\circ 23' & 0.307 \\ 47^\circ 55' & 0.286 \\ 50^\circ 26' & 0.287 \\ 52^\circ 58' & 0.287 \\ 52^\circ 58' & 0.287 \\ 55^\circ 30' & 0.279 \\ 58^\circ 02' & 0.263 \\ 60^\circ 33' & 0.242 \\ 63^\circ 04' & 0.206 \\ 65^\circ 35' & 0.172 \\ 68^\circ 07' & 0.146 \\ 70^\circ 38' & 0.132 \\ 73^\circ 09' & 0.134 \\ 75^\circ 39' & 0.130 \\ 78^\circ 10' & 0.154 \\ 80^\circ 40' & 0.165 \\ 88^\circ 11' & 0.165 \\ 88^\circ 11' & 0.165 \\ \end{array}$

TABLE I. $(\sigma/\sigma_R)_{c.m.}$ vs $\theta_{c.m.}$ for 15-Me	V deuterons elastically scattered from sever	al elements (continued).

Rh	Pd	Ag	Cd	In	Sn ¹²⁰
$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$	$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$	$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$	$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$	$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$	$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$
20° 15' 0.979 22° 48' 1.10 25° 21' 0.952 27° 54' 0.842 30° 26' 0.815 32° 59' 0.791 35° 31' 0.745 38° 04' 0.695 40° 36' 0.660 43° 08' 0.599 45° 40' 0.547 48° 12' 0.491 50° 44' 0.449 53° 16' 0.388 55° 48' 0.365 58° 20' 0.338 60° 51' 0.309 63° 22' 0.296 65° 53' 0.299 68° 25' 0.294 70° 56' 0.293 73° 27' 0.296 75° 58' 0.290 78° 29' 0.215 85° 59' 0.183 88° 29' 0.156 90° 59' 0.140	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 19^{\circ} 40' & 1.01\\ 22^{\circ} 13' & 0.998\\ 24^{\circ} 46' & 0.835\\ 27^{\circ} 18' & 0.695\\ 29^{\circ} 50' & 0.629\\ 32^{\circ} 22' & 0.569\\ 34^{\circ} 55' & 0.530\\ 37^{\circ} 27' & 0.510\\ 39^{\circ} 59' & 0.476\\ 42^{\circ} 31' & 0.437\\ 45^{\circ} 03' & 0.393\\ 47^{\circ} 35' & 0.355\\ 50^{\circ} 07' & 0.326\\ 52^{\circ} 39' & 0.310\\ 55^{\circ} 10' & 0.296\\ 57^{\circ} 41' & 0.279\\ 60^{\circ} 13' & 0.254\\ 62^{\circ} 45' & 0.229\\ 65^{\circ} 16' & 0.213\\ 67^{\circ} 47' & 0.200\\ 70^{\circ} 18' & 0.188\\ 72^{\circ} 49' & 0.197\\ 75^{\circ} 20' & 0.187\\ 77^{\circ} 50' & 0.182\\ 80^{\circ} 20' & 0.174\\ 82^{\circ} 55' & 0.140\\ 90^{\circ} 21' & 0.125\\ \end{array}$	20° 22' 1.02 22° 53' 0.845 25° 26' 0.745 27° 58' 0.712 30° 30' 0.646 33° 02' 0.585 35° 35' 0.560 38° 07' 0.540 40° 39' 0.490 43° 11' 0.483 45° 43' 0.433 48° 15' 0.387 50° 47' 0.347 53° 19' 0.343 55° 50' 0.311 58° 31' 0.282 60° 53' 0.263 63° 25' 0.224 70° 58' 0.218 73° 29' 0.213 76° 00' 0.202 83° 30' 0.172 86° 01' 0.159 88° 31' 0.140 91° 01' 0.121	$\begin{array}{c} 20^{\circ} 04' & 1.02\\ 22^{\circ} 35' & 1.00\\ 25^{\circ} 08' & 0.880\\ 27^{\circ} 40' & 0.762\\ 30^{\circ} 12' & 0.714\\ 32^{\circ} 44' & 0.665\\ 335^{\circ} 17' & 0.581\\ 37^{\circ} 49' & 0.559\\ 40^{\circ} 21' & 0.504\\ 42^{\circ} 53' & 0.465\\ 45^{\circ} 25' & 0.438\\ 47^{\circ} 57' & 0.397\\ 50^{\circ} 29' & 0.380\\ 53^{\circ} 01' & 0.365\\ 55^{\circ} 32' & 0.352\\ 58^{\circ} 03' & 0.225\\ 60^{\circ} 35' & 0.291\\ 63^{\circ} 07' & 0.257\\ 65^{\circ} 48' & 0.223\\ 68^{\circ} 09' & 0.204\\ 70^{\circ} 40' & 0.186\\ 73^{\circ} 11' & 0.188\\ 75^{\circ} 42' & 0.193\\ 78^{\circ} 12' & 0.200\\ 80^{\circ} 42' & 0.207\\ 83^{\circ} 12' & 0.196\\ 85^{\circ} 43' & 0.141\\ 90^{\circ} 43' & 0.141\\ \end{array}$	20° 22' 1.08 22° 54' 0.956 22° 54' 0.956 25° 27' 0.804 27° 59' 0.703 30° 31' 0.644 33° 03' 0.702 35° 35' 0.636 38° 07' 0.650 40° 39' 0.608 43° 10.644 50° 40' 0.30' 0.702 35° 35' 0.636 38° 07' 0.650 40° 39' 0.608 43° 10.500 48° 15' 0.440 50° 46' 0.387 53° 19' 0.347 55° 49' 0.307 58° 21' 0.290 60° 52' 0.285 63° 22' 0.275 68° 25' 0.293 70° 56' 0.281 73° 26' 0.272 75° 57' 0.261 78° 27' 0.233 80° 58' 0.206 83° 28' 0.171 85° 59' 0.153 88° 28' 0.135 90° 59' 0.128 93° 49' 0.127 96° 19' 0.139 98° 48' 0.138 10° 17' 0.108 108° 46' 0.083 111° 18' 0.133 103° 44' 116° 13' 0.059
	$\operatorname{Er}(q(q_{1}))$	θ (σ	Yb	T A (r	a
	709 291 0 250	109.27/ 1.05	709 01/ 0 204	109 57/ 105	/ V K/c.m.
$\begin{array}{c} 20 & 14 \\ 22^{\circ} & 46' & 1.05 \\ 25^{\circ} & 17' & 1.00 \\ 27^{\circ} & 49' & 1.03 \\ 30^{\circ} & 20' & 0.97 \\ 32^{\circ} & 51' & 0.89 \\ 35^{\circ} & 23' & 0.83 \\ 37^{\circ} & 54' & 0.80 \\ 40^{\circ} & 26' & 0.735 \\ 42^{\circ} & 57' & 0.675 \\ 42^{\circ} & 57' & 0.675 \\ 42^{\circ} & 57' & 0.675 \\ 45^{\circ} & 29' & 0.577 \\ 48^{\circ} & 00' & 0.520 \\ 50^{\circ} & 31' & 0.463 \\ 53^{\circ} & 02' & 0.439 \\ 55^{\circ} & 33' & 0.414 \\ 58^{\circ} & 04' & 0.404 \\ 60^{\circ} & 35' & 0.370 \\ 63^{\circ} & 06' & 0.332 \\ 65^{\circ} & 37' & 0.326 \\ 68^{\circ} & 08' & 0.302 \end{array}$	73° 00' 0.278 73° 00' 0.254 75° 39' 0.238 78° 10' 0.211 80° 40' 0.199 83° 10' 0.193 85° 40' 0.184 88° 10' 0.173 90° 40' 0.167	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	72° 32' 0.265 75° 02' 0.262 77° 33' 0.238 80° 03' 0.224 82° 33' 0.220 85° 03' 0.209 87° 33' 0.189 90° 03' 0.194	$\begin{array}{c} 10 \\ 21^{\circ} 29' \\ 1.13 \\ 24^{\circ} 00' \\ 1.11 \\ 26^{\circ} 32' \\ 1.09 \\ 29^{\circ} 03' \\ 1.05 \\ 31^{\circ} 34' \\ 0.903 \\ 34^{\circ} 06' \\ 0.858 \\ 36^{\circ} 37' \\ 0.782 \\ 39^{\circ} 08' \\ 0.762 \\ 41^{\circ} 40' \\ 0.733 \\ 44^{\circ} 11' \\ 0.649 \\ 46^{\circ} 42' \\ 0.605 \\ 49^{\circ} 13' \\ 0.577 \\ 51^{\circ} 45' \\ 0.525 \\ 54^{\circ} 15' \\ 0.473 \\ 54^{\circ} 15' \\ 0.473 \\ 54^{\circ} 15' \\ 0.473 \\ 59^{\circ} 17' \\ 0.453 \\ 61^{\circ} 48' \\ 0.421 \\ 64^{\circ} 18' \\ 0.380 \end{array}$	09 19 0.349 71° 50' 0.320 74° 20' 0.292 76° 51' 0.276 79° 21' 0.261 81° 52' 0.248 84° 22' 0.237 86° 53' 0.230 89° 23' 0.221

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W	Pt	Au	Pb
$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$	$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$	$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$	$\theta_{\rm c.m.}$ $(\sigma/\sigma_R)_{\rm c.m.}$
$\begin{array}{c cccc} & & & & & & \\ \hline & & & & & & \\ \hline & & & &$	$\begin{array}{c cccc} & & & & & & & & & & & & & & & & & $	Au $\theta_{c.m.}$ $(\sigma/\sigma_R)_{c.m.}$ 20° 06′ 1.00 22° 37′ 1.00 25° 09′ 1.03 27° 40′ 1.02 30° 11′ 1.00 32° 42′ 0.948 35° 13′ 0.917 37° 44′ 0.862 40° 22′ 0.828 42° 53′ 0.801 45° 24′ 0.741 47° 55′ 0.705 50° 26′ 0.665 52° 57′ 0.663 55° 28′ 0.601 57° 59′ 0.505 60° 30′ 0.458 63° 00′ 0.436 65° 31′ 0.405 68° 01′ 0.381 70° 32′ 0.377 73° 02′ 0.364 75° 33′ 0.331	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccc} 78^{\circ}06' & 0.272 \\ 80^{\circ}37' & 0.257 \\ 83^{\circ}07' & 0.249 \\ 85^{\circ}37' & 0.231 \\ 88^{\circ}08' & 0.228 \\ 90^{\circ}38' & 0.218 \end{array}$	$\begin{array}{cccccc} 76^\circ \ 48' & 0.321 \\ 79^\circ \ 18' & 0.301 \\ 81^\circ \ 49' & 0.286 \\ 84^\circ \ 19' & 0.256 \\ 86^\circ \ 49' & 0.237 \\ 89^\circ \ 19' & 0.229 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

TABLE I. $(\sigma/\sigma_R)_{e.m.}$ vs $\theta_{e.m.}$ for 15-MeV deuterons elastically scattered from several elements (continued).

controlled, so that during the course of the experiments reported here it may have varied between 14.6 and 15.0 MeV. The variations during a measurement of a single angular distribution, however, are an order of magnitude smaller than this. Tests were made to ascertain that beam misalignment or scattering in the target do not cause errors in the Faraday cup beam current measurement even for the thickest and heaviest targets. The current integrator was frequently checked with a known current from a standard electrolytic cell.

Variations in target thickness (from the average value



FIG. 2. Typical 15-MeV deuteron elastic scattering angular distribution data in the mass region A = 25 to 60. Data points were taken at intervals of 2.5°. Ordinates are the ratios of total to Rutherford cross section at the scattering angles $\theta_{c.m.}$, which are the abscissas (in center-of-mass the system). Each point is the average of two or three independent experimental determinations. The scatter of the adjacent points tells the size of errors in the experiment.

calculated from the total area and mass) was a particularly difficult problem in some cases; this was checked by use of several different targets of the same element.

The angle of the incident beam was checked frequently by measuring elastic scattering from a heavy element (target Au or Pt) at equal angles on each side of the nominal 0° and a zero angle correction was obtained from the intensity ratio between the two measurements by use of the Rutherford formula as follows: If the ratio of count rates at $+20^{\circ}$ and -20° (where these angles are measured from the nominal 0°) is R, the correction in degrees to the zero angle, Δ , is given by $\Delta = 2.5$ (1-R). The zero angle varied from day to day by less than $\frac{1}{2}$ deg, and was uncertain by less than $\frac{1}{4}$ deg. The acceptance angle for scattered particles was usually 2°, but in some cases it was less. Errors in setting the scattering angle and in alignment were negligible. A detailed discussion of errors in experiments of this type has been given by Low.6

The most important errors due to angular uncertainties are eliminated by the method of determining absolute cross sections. This was done by normalizing all measurements to those for Pt at 20° and 25°, and assuming the Pt cross sections to be given correctly by the Rutherford formula at these small angles as is expected from optical model calculations. This method eliminates errors not only from angular uncertainties but from uncertainties in the geometry of the system

 $^{\rm 6}$ C. A. Low, M.S. thesis, University of Pittsburgh, 1960 (unpublished).

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arising from vertical bending by the fringe fields of the magnet.

Errors from imperfect performance of electronic instrumentation were checked by simultaneously feeding the signal from the center crystal into two different amplifier-discriminator-scalar systems. Results from the two systems were recorded in all runs. The scalars had 100 kC and 10 MC maximum count rates, respectively, so that errors due to excessive count rates were immediately detected. In all cases, count rates were kept conservatively low, but the lengths of runs were adjusted to give 1% statistical accuracy. Measurements were made at 2.5° intervals between 20° and 90° for all targets, and up to 140° for Ni, Zr, Sn¹²⁰, and Pb. All angular distributions were measured at least twice on separate days (many were done three or more times) and in no case was there a significant discrepancy in the shape of the angular distributions. There were discrepancies in the determinations of absolute cross sections, so that a large number of separate runs were made to check

FIG. 4. Typical data in the mass re-gion A = 180 to 200. (See also caption for Fig. 2.)

Fig. 2.)



absolute cross sections at 20° and 25°. The discrepancies were found to be due to variations in thickness of the Au foils used for the early calibrations, so that Pt was used for calibrations in the later work.

RESULTS AND DISCUSSION

The values of $(\sigma/\sigma_R)_{c.m.}$ at different values of $\theta_{c.m.}$ for the different elements studied in the present work



are given in Table I. Typical data picked from throughout the entire range of investigation are presented in Figs. 2-4. Figure 5 presents smooth curves drawn through the data points for all the elements and put together closely for studying the systematic and singular changes in structure as one goes through the periodic table. Such features as are immediately obvious from an examination of Fig. 5, are discussed below:

(1) (σ/σ_R) vs θ shows oscillations that are quite sharp in light nuclei but are increasingly damped as the mass increases. The oscillations are the well-known diffraction effect; their damping with increasing mass is well

known from other elastic scattering angular distribution experiments and can be explained by the volume absorption model⁷ by changing the depth of the imaginary potential with nuclear mass, or by the surface absorption model⁸ where it follows from the decrease in surface to volume ratio with mass.

(2) Maxima and minima of the distribution shift to smaller angles with increasing A as one expects from Fraunhofer diffraction theory, according to which⁹

$$(d\sigma/d\Omega)_{\text{Elastic}} = (Kr^2)^2 [J_1(qr)/qr]^2, \qquad (1)$$

where J_1 is the first-order Bessel function, r is the interaction radius, K is the momentum of the incident particle, and q is the momentum transfer which, for elastic scattering, is

$$q = 2K\sin(\theta/2).$$
 (2)

It is clear from (1) that the oscillations in the angular distributions arise from the Bessel function, so that the location of maxima and minima should depend only on the argument of the Bessel function, qr, which is proportional to $A^{1/3}\sin(\theta/2)$. To test this, the value of $A^{1/3}\sin(\theta/2)$ for each maximum and minimum in the angular distributions is plotted vs A in Fig. 6. According to the theoretical discussion above, the points in Fig. 6 lie along horizontal lines; this expectation is at least roughly fulfilled.

(3) Perhaps the most surprising feature of Fig. 5 is the few cases where there is a sharp change of angular distribution pattern over a small mass change. The most striking situation of this type is between Nb⁹³ and Mo which has an average mass of 96. Another almost equally striking change is that between In¹¹⁵ and Sn¹²⁰. There are also striking differences between In¹¹⁵ and Cd (av A = 112), between Rh¹⁰³ and Pd (av A = 106), and between Ni and Cu (av A = 59 and 64, respectively). Such sharp changes are clearly contra-



FIG. 6. Systematics of positions of maxima and minima from Fig. 5. The ordinate is $A^{1/3} \sin(\theta/2)$ and the abscissa is A, where θ is the scattering angle and A is the mass number of the scatterer.



FIG. 7. The angular distributions of Ti, Ni, Rh, Sn, and Pb taken from the references indicated in the legend.

dictory to the basic assumptions of the optical model, and should be studied further.

(4) σ/σ_R averaged over the oscillations decreases with θ in all elements. The slope is mild in Al but gets large in medium and heavy elements though the change in slope is not very perceptible in the mass region A = 60-200. Variations with mass in the aforesaid slope are much larger in $(p,p)^{10}$ and $(\alpha,\alpha)^{11}$ elastic scattering angular distributions.

A comparison with the 11.8 MeV data of Igo *et al.*¹ shows essential agreement with this data and the expected shift of peaks and valleys to smaller angles relative to their angular distributions. There are, however, discrepancies with the 15 MeV data of Cindro and Wall² in that the angular distributions for Rh and Pd, and for Cu and Fe are found to be similar in this work.

Some information on the energy dependence of elastic deuteron scattering is shown in Fig. 7, where data from references 1–3 are compared with this work. In general, the energy dependence is slowly varying, but there are a few nontrivial differences. For example, the minimum in the nickel angular distribution at $\sim 70^{\circ}$ does not appear at other energies.

An optical-model analysis of the data presented here is in progress.¹²

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⁷ R. D. Woods and D. S. Saxon, Phys. Rev. **95**, 577 (1954). ⁸ F. E. Bjorklund, S. Fernbach, and N. Sherman, Phys. Rev. **101**, 1832 (1956).

⁹ See, for example, J. S. Blair, Phys. Rev. 115, 928 (1959).

¹⁰ B. L. Cohen and R. V. Neidigh, Phys. Rev. **93**, 282 (1954). ¹¹ I. S. Shapiro, Usp. Fiz. Nauk **75**, 61 (1961) [translation: Soviet Phys.—Usp. **4**, 674 (1962)].

¹² R. M. Drisko (private communication).